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**NANOCELLULOSE-REINFORCED PHENOL-FORMALDEHYDE RESIN FOR  
PLYWOOD PANEL PRODUCTION**

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**ABSTRACT**

The search for new technologies to improve adhesives and the properties of reconstituted wood panels is constant, and nanotechnology is a tool for this purpose. The aim of this study is investigating the effect of adding nanocellulose in the formulation of the adhesive phenol-formaldehyde on the physico-mechanical properties of *Pinus taeda* plywood panels. Three ratios of nanofibrillated cellulose (NFC) were added to the adhesive formulation used to produce plywood panels: 0,026 %, 0,038 % or 0,064 %. The panels were tested according to the European standards; apparent density, resistance to parallel and perpendicular flexure and glue line shear strength were determined after 6 hours of boiling and after the boiling cycle for the 1<sup>st</sup> glue line (face) and 2<sup>nd</sup> line (core). The use of NFC in the adhesive caused an increase of viscosity and reduction of the gel time of the adhesive. The apparent density of the panels was not influenced by the addition of NFC, but the properties of parallel bending, perpendicular flexing and glue line shear were sensitive to the addition of NFC. The NR2 treatment (0,038 % NFC) presented the best results in the mechanical tests.

**Keywords:** Glue line shear test, mechanical properties, nanotechnology, nanofibrillated cellulose, plywood.

## INTRODUCTION

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The use of solid wood presents some disadvantages because it is heterogenous and anisotropic (Torquato 2002; Fratzl and Weinkamer 2007; Buligon 2015), and in many cases the mechanical properties of wood are unsatisfactory for certain uses (Song *et al.* 2018). In addition, due to natural defects or the tree's own growth, there is a limitation of dimensions for many uses (Maloney 1993). Therefore, the production of wood panels can be a more rational use of this raw material (Carvalho 2016).

Wood panels are composites that use wood and adhesives as bonding agents, to improve the characteristics of the raw material (Lengowski *et al.* 2019). Plywood panels are composed of overlapping wood sheets bonded with adhesives, mainly phenol-formaldehyde and urea-formaldehyde, under high pressure and temperature, with the fibers (grain) crossed at an angle of 90° (Yuce *et al.* 2014).

Resin represents the third highest industrial cost, which leads to constant research for improved adhesives in terms of performance and economy (Eichhorn *et al.* 2010; Gindl-Altmatter and Veigel 2014). One kind of improvement is the reinforcement of adhesives with nanocellulose. Resin reinforced with nanocellulose has been identified as promising, among various improvements offered by nanotechnology in the forest products industry (Candan and Akbulut 2015). Various applications have provided improvement in both the physical and mechanical properties of panels (Gindl-Altmatter and Veigel 2014).

Nanocelluloses are cellulosic materials having at least one dimension in nanometric scale. Nanocelluloses can be produced by different methods and from various lignocellulosic sources (Abdul Khalil *et al.* 2014). Nanofibrillated cellulose (NFC) is a kind of nanocellulose produced by a homogenization or grinding process, with diameter between 5 nm and 30 nm and amorphous and crystalline zones composing their structure (Sehaqui *et al.* 2011; Rojas *et al.* 2015; Samyn *et al.* 2018). Due to the small size, nanomaterial has properties such as high aspect

61 ratio, crystallinity and surface area, excellent mechanical properties combined with less weight,  
62 along with better biodegradability than solid wood (Eichhorn *et al.* 2010; Mondragon *et al.*  
63 2015).

64 Therefore, this work evaluates the effect of NFC addition on the phenol-formaldehyde  
65 adhesive and the physico-mechanical properties of *Pinus taeda* plywood panels.

## 66 MATERIAL AND METHODS

### 67 Material

68 The panels were made by Dallo Madeiras Ltda., a company located in the city of Três  
69 Barras, Santa Catarina, Brazil. The analysis and production of nanofibrillated cellulose (NFC)  
70 as well as the quality tests of the adhesives and panels were carried out at Federal University of  
71 Paraná.

72 The nanocellulose used was NFC dispersed in 1 % aqueous solution, produced from  
73 bleached cellulose of *Eucalyptus* sp. It has a mean diameter of 22,28 nm and a variable length  
74 in the micrometer scale, considered as nanomaterial and nano-object according to ISO standards  
75 ISO/TS 20477:2017 (ISO 2017).

76 The phenol-formaldehyde resin used was produced by the company Hexion and marketed  
77 under the name Cascophen HL-7090 Hs, with solids content of 52,4 %, gel time at 121 °C of 8  
78 minutes, pH of 12 and Brockfield viscosity of 455 cp (LVF 2 / 60/25 °C). In addition to the  
79 resin, wheat flour was used as extender, with Ford viscosity cup number 8 of 25 seconds.

80 The veneers used are produced from *Pinus taeda* wood with 2,8 mm thickness dried in  
81 an industrial dryer until reaching average moisture content of 8 % in the core and 12 % on the  
82 face, the higher moisture content in the face veneers are needed to allow heat conduction from  
83 the press into the panel and also to prevent pre-curing of the adhesive.

### 84 Adhesive formulation and characterization

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87 The solids content of the adhesive was set at 26,7 % for all compositions. The phenol-  
88 formaldehyde resin, extender, water and NFC were used to compose the adhesive according to  
89 the formulations described in Table 1.

90 **Table 1:** Adhesive formulations.

Component	CA	NR1	NR2	NR3
Resin (%)	50,640	50,640	50,640	50,640
Extender (%)	23,820	23,820	23,820	23,820
Water (%)	25,640	25,614	25,602	25,576
NFC (%)	0,000	0,026	0,038	0,064

91 CA: control adhesive; NR: nano-reinforced adhesive.

92 For viscosity determination, a Ford Cup #8 was used, in which the cup was filled with the  
93 adhesive and the flow time was measured until the first interruption in the flow through the bore  
94 of the cup, in accordance with ASTM D1200-18 (ASTM 2018).

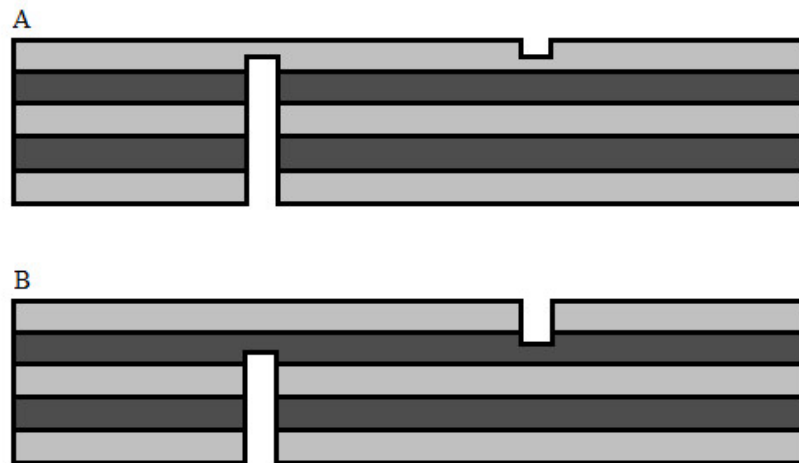
95 About 1,0 g of adhesive was placed in a 15,0 cm x 2,0 cm test tube, which was dipped in  
96 a glycerin bath at 120 °C. The gelatinization time for each adhesive sample was measured from  
97 dipping in the glycerin bath until partial adhesive hardening, verified when it offered greater  
98 resistance to the rotation of the glass stick, in accordance with ASTM 2471-99 (ASTM 1999).

99 The pH was determined with a digital pHmeter, at a temperature of 25 °C, calibrated to  
100 pH 4 and 7 using standard buffer solutions. Approximately 200 mL of the adhesives was used  
101 in three replicates, following the E70-07 standard (ASTM 2015).

### 102 **Production and characterization of panels**

103 The wood veneers of *Pinus taeda* used had dimensions of 600 mm x 600 mm x 2,8 mm.  
104 The panels were produced with five layers, the resins being applied to one side of the veneer  
105 with a weight of 380 g·cm<sup>-2</sup> (double line). The panels were pressed at a temperature of 140 °C,  
106 with specific pressure of 11 kgf·cm<sup>-2</sup> for 12 minutes. Three panels were produced per treatment,  
107 totaling 12 panels analyzed.

108 After pressing, the panels were conditioned in a climatic chamber at a temperature of 20  
109 °C ± 3 °C and relative humidity of 65 % ± 5 %. The samples for tests of apparent density, static  
110 (parallel and perpendicular) flexure and glue line shearing (dry test, 6 hours' boiling and boiling  
111 cycle) were cut according to the requirements of EN 323, 310 and 314 (CEN, 1993a, b, c). The  
112 shear tests were performed on the 1<sup>st</sup> (face) and 2<sup>nd</sup> (core) glue line (Figure 1).



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114 **Figure 1:** Side view of the test specimens for the glue line shear test. A: 1<sup>st</sup> glue line, B: 2<sup>nd</sup>  
115 glue line.

### 116 **Data analysis**

117 Tests of homogeneity and analysis of variance (ANOVA) were performed, and when  
118 significant difference was detected between treatments, the Tukey test was used, at 5 %  
119 significance. The data were analyzed with the statistical software Statgraphics (2019).

## 120 **RESULTS AND DISCUSSION**

### 121 **Adhesive characterization**

122 The mean results of the control adhesive and adhesives reinforced with NFC are shown  
123 in Table 2.  
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125 The addition of nanocellulose to the adhesives affected significantly the physico-chemical  
126 properties, except for pH, which remained practically constant for all adhesives ( $p$ -value =  
127 0,0521). In general, the percentage increase of nanocellulose in the adhesives caused an increase  
128 significant in the viscosity ( $p$ -value = 0,0000) and decrease in the gel time ( $p$ -value = 0,0000).

129 **Table 2:** Properties of control adhesive and adhesives with different additions of NFC.

Property	CA	NR1	NR2	NR3
Viscosity (s)	127 a (1,57)	69 b (4,35)	63 c (1,58)	53 d (1,08)
Gel time (s)	518 a (2,52)	384 b (2,36)	363 bc (0,57)	349 c (5,29)
pH	11,7 a (1,77)	12,2 a (1,64)	12,1 a (1,72)	11,8 a (0,85)

130 CA: control adhesive; NR: nano-reinforced adhesive. Means followed by the same letter in the column are  
 131 statistically the same by the Tukey test at 95 % confidence; values in parentheses indicate the coefficient of  
 132 variation.

133 Viscosity is one of the most important properties of an adhesive (Din *et al.* 2018), and  
 134 this feature depends on the temperature (generally decreasing with rising temperature of the  
 135 liquid) and its composition (Peschel *et al.* 2016). The viscosity of the adhesive increased with  
 136 the addition of NFC: for NR1, the viscosity increased by 45 %, for NR2 by 50 % and for NR3  
 137 by 58 % in relation to the control sample, indicating that small amounts of NFC modify this  
 138 property. The viscosity of fluids comes from the internal friction of the particles, which are  
 139 influenced by the forces of attraction between molecules. Since NFC has many free hydroxyl  
 140 groups to form bonds, the force of attraction influenced the viscosity. The increase in viscosity  
 141 has a negative influence on the penetration of the adhesive, so that when the viscosity is high,  
 142 the uniform distribution of the adhesive on the wood is difficult, with insufficient penetration  
 143 into the wood structure, impairing wetting and leaving a line of thick glue with low mechanical  
 144 resistance (Gonçalves and Lelis 2009).

145 Mahrtdt *et al.* (2016) and Cui *et al.* (2014) found that the addition of nanocelulose in urea-  
 146 formaldehyde resin caused an increase in the viscosity of the adhesive, a result similar to the  
 147 one found in this work. Damásio *et al.* (2017), Ferreira (2017) and Liu *et al.* (2015) observed a  
 148 change in the viscosity of adhesives with addition of nanocrystalline cellulose (CNC), and this  
 149 change was linked only to the physical interaction between the adhesive and the nanocelulose,  
 150 since no chemical reaction between the adhesive and CNC was observed. According to Gindl-  
 151 Altmutter and Veigel (2014), the large increase of the viscosity caused by the addition of  
 152 nanocelulose can represent a serious obstacle to resin spraying and impregnation in the wood.

153 The gel time of the adhesives changed with increasing NFC content, with reductions of  
154 26 % for adhesive NR1, 32 % for NR2 and 33 % for NR3 relative to the control adhesive. The  
155 addition of NFC caused a decrease in the gel time, indicating that the working time of the  
156 adhesives was reduced and that a shorter pressing time would be required for cure of the  
157 adhesive. Shorter working time makes it harder to apply and spread the adhesive in the wood  
158 due to its rapid polymerization, causing a decrease in the strength of the glue line (Cunha 2016).  
159 In industrial settings, shorter gel times are aimed at reducing the pressing time, resulting in  
160 increased productivity and reduced energy consumption.

161 Cui *et al.* (2014) produced nanofibrillated cellulose (NFC) reinforced particle boards and  
162 observed increased gel time of a tannin-based adhesive with the addition of NFC (1 % to 3 %).  
163 Mahrtdt *et al.* (2016) found a delay in the formation of the chemical and mechanical bonding  
164 during resin curing, unlike what was found here for phenol-formaldehyde resin. However, they  
165 also found that the addition of MFC allowed better distribution of the adhesive in the wood,  
166 with less formation of clots (which weakens the bond), besides presenting the same penetration  
167 in the wood.

168 The pH of the adhesives remained practically constant, preserving the chemical  
169 characteristic of the adhesive used. Since the mechanical production of NFC occurs only with  
170 the addition of water, the pH of NFC does not change. Unlike the use of CNC, which because  
171 acids are used in their production have a slightly acid charge, the addition of NFC can delay or  
172 accelerate the cure depending on the adhesive type, due to the change of pH (Gindl-Altmutter  
173 and Veigel 2014).

#### 174 **Plywood characterization**

175 Table 3 shows the average results of the specific gravity at 12 % moisture of the plywood  
176 obtained from the different treatments.

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**Table 3:** Mean results of specific gravity of plywood.

Treatment	Specific gravity ( $\text{kg}\cdot\text{m}^{-3}$ )
CA	486 a (4,5)
NR1	477 a (4,8)
NR2	476 a (6,1)
NR3	457 a (5,8)

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CA: control adhesive; NR: nano-reinforced adhesive. Means followed by the same letter in the column are statistically the same by the Tukey test at 95 % confidence; values in parentheses indicate the coefficient of variation.

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The specific gravity of the plywood did not show significant variation after the addition of the NFC in the adhesive ( $p$ -value = 0,0635).

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The specific gravity of plywood is related to the density of the raw material, the adhesive solids content, as well as amount of resin in the glue line. Since there was no variation in the adhesive solids and the amount of resin placed in each treatment, the variation found was associated with the variability in the density of the *Pinus taeda* veneers. The specific gravity produced was below the specific gravity of the panels produced with 100 % *Pinus taeda* by Iwakiri *et al.* (2018), which presented specific gravity of  $600 \text{ Kg}\cdot\text{m}^{-3}$ , and ABIMCI (2017) for commercial *Pinus* plywood, from 490 to  $560 \text{ kg}\cdot\text{m}^{-3}$ . This result is related to the quality of the raw material: wood with higher specific gravity results in panels with higher specific gravity (Iwakiri *et al.* 2012).

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Table 4 shows the average results of the parallel and perpendicular static bending of the plywood obtained for the different treatments.

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Statistical difference was observed between the parallel static bending treatments for MOE ( $p$ -value = 0,0128) and MOR ( $p$ -value = 0,0027). The mean values of MOE and MOR strength for parallel static bending ranged from 4425,27 MPa to 2734,60 MPa and from 37,74 MPa to 24,23 MPa. The parallel static bending strength of the panels was statistically equal to the control for the NR1 and NR2 treatments, demonstrating that the bonding was not impaired with the addition of the NFC in these treatments. However, a significant reduction of 38,18 %



202 in these properties was observed for the treatment with highest addition of NFC in the glue  
 203 composition (NR3). On perpendicular static bending, a statistically significant difference was  
 204 observed between the treatments for the MOE (p-value = 0,0091) while the MOR showed no  
 205 significant difference (p-value = 0,1149). For perpendicular static bending, the MOE ranged  
 206 between 1599,54 MPa and 1146,00 MPa and MOR between 22,54 MPa and 17,04 MPa. For  
 207 this analysis, only MOE presented statistical difference, where the NR1 treatment was equal to  
 208 the control treatment and the lowest values for this property were found for the highest levels  
 209 of NFC addition (NR2 and NR3).

210 **Table 4:** Mean results of static bending test of plywood.

Treatment	Parallel		Perpendicular	
	MOE (MPa)	MOR (MPa)	MOE (MPa)	MOR (MPa)
CA	4425,27 a (14,7)	36,62 a (14,9)	1599,54 a (13,5)	21,22 a (15,5)
NR1	3440,45 ab (23,4)	32,74 ab (20,6)	1263,02 ab (16,6)	19,14 a (28,9)
NR2	3301,27 ab (25,2)	37,74 a (13,4)	1146,00 b (20,4)	17,04 a (10,3)
NR3	2734,60 b (24,9)	24,23 b (22,1)	1196,22 b (19,3)	22,54 a (18,6)

211 CA: control adhesive; NR: nano reinforced adhesive. MOE: modulus of elasticity; MOR: modulus of rupture.  
 212 Means followed by the same letter in the column are statistically the same by the Tukey test at 95 % confidence;  
 213 values in parentheses indicate the coefficient of variation.

214 The parallel static bending results for the NR1 and NR2 treatments were statistically equal  
 215 to the control (CA), demonstrating that the bonding was not impaired with the addition of NFC.  
 216 Adding a higher NFC content (NR3) impaired the parallel static bending. For resistance to  
 217 perpendicular static bending, the MOE of the NR1 treatment was equal to the control treatment  
 218 (CA), whereas the MOR was statistically equal in all treatments.

219 Besides the specific gravity, the static bending of plywood panels is influenced by the  
 220 quality of the raw material used in the production of the veneers. Wood with higher specific  
 221 gravity results in panels with greater resistance to static bending (Iwakiri *et al.* 2012). The  
 222 values found in this work are below those reported by Ross (2010), which states that the parallel  
 223 MOE of *Pinus* sp. is 7700 MPa and the parallel MOR is 37,09 MPa. The values found are also

224 below the values reported by ABIMCI (2017) for plywoods of *Pinus* sp. marketed in Brazil, for  
 225 which parallel MOE varies between 4876 MPa and 8921 MPa; parallel MOR between 23,4  
 226 MPa and 52,7 MPa; perpendicular MOE between 1903 MPa and 3774 MPa; and perpendicular  
 227 MOR between 15,8 MPa and 34,8 MPa.

228 Table 5 shows the average values of glue line shear strength in the dry tests, after 6 hours  
 229 of boiling and the boiling cycle of the plywood samples.

230 **Table 5:** Mean results of glue line shear strength.

Treatment	Shear strength - dry (MPa)		Shear strength - 6 h (MPa)		Shear strength - cycle (MPa)	
	Core	Face	Core	Face	Core	Face
CA	1,32 b (17,4)	1,28 ab (22,4)	1,20 b (32,4)	0,75 a (25,9)	0,98 c (42,0)	0,64 a (37,6)
NR1	2,45 a (22,3)	1,30 ab (22,1)	1,31 ab (28,7)	0,63 a (42,3)	1,00 bc (36,7)	0,49 a (49,9)
NR2	2,30 a (23,9)	1,50 a (23,9)	1,37 ab (36,7)	0,72 a (25,5)	1,42 a (30,3)	0,63 a (45,3)
NR3	2,26 a (13,4)	1,09 b (23,6)	1,55 a (24,3)	0,58 a (35,9)	1,33 ab (28,7)	0,70 a (25,9)

231 CA: control adhesive; NR: nano reinforced adhesive. Means followed by the same letter in the column are  
 232 statistically the same by the Tukey test at 95 % confidence; values in parentheses indicate the coefficient of  
 233 variation.

234 The average shear strength values in the dry tests for the 1<sup>st</sup> glue line varied from 1,09  
 235 MPa (NR3) to 1,950 MPa (NR2), while for 2<sup>nd</sup> glue line it varied between 1,32 MPa (AC) and  
 236 2,45 MPa (NR2). The percentages of failure of the wood varied from 63 % to 89 % for the 1<sup>st</sup>  
 237 glue line and from 69 % to 95 % for the 2<sup>nd</sup> glue line. Although the treatments of core ( $p$ -value  
 238 = 0,000) and face ( $p$ -value = 0,0063) presented statistical difference between them, all  
 239 treatments presented average shear strength values above the minimum value of 1,0 MPa  
 240 established by EN 314-2 (CEN 1993b).

241 After boiling for 6 hours, the average shear values varied for the 1<sup>st</sup> glue line from 0,58  
242 MPa (NR3) to 0,75 MPa (CA) and for the 2<sup>nd</sup> glue line ranged between 1,20 MPa (CA) and  
243 1,55 MPa (NR3). The percentages of failure in the wood varied from 16 % to 32 % for the 1<sup>st</sup>  
244 glue line and from 60 % to 83 % for the 2<sup>nd</sup> glue line. Only the core glue line test result met the  
245 requirements laid down in EN 314-2 (CEN 1993b). Statistically there were differences between  
246 treatments for the 2<sup>nd</sup> glue line ( $p$ -value = 0,0421), whereas for the 1<sup>st</sup> glue line the treatments  
247 were statistically similar ( $p$ -value = 0,0555).

248 The shear strength after the boiling cycle varied for the 1<sup>st</sup> glue line from 0,49 MPa (NR1)  
249 to 0,70 MPa (NR3) and for the 2<sup>nd</sup> glue line from 0,98 MPa (CA) to 1,42 MPa (NR2). The  
250 percentages of faults in the wood ranged from 20 % to 39 % for the 1<sup>st</sup> glue line and from 47 %  
251 to 69 % for the 2<sup>nd</sup> glue line. Again, only the core glue line result met the requirements laid  
252 down in EN 314-2 (CEN 1993b). Statistically the behavior was similar to the pre-treatment of  
253 6 hours of boiling, in which there was difference between treatments for the tests of the 2<sup>nd</sup> line  
254 of glue ( $p$ -value = 0,0013) whereas for the 1<sup>st</sup> glue line the treatments were statistically equal  
255 ( $p$ -value = 0,1061).

256 There was improvement in shear strength of the glue line with the addition of  
257 nanocellulose to the 2<sup>nd</sup> glue line, whereas for the 1<sup>st</sup> glue line only the dry test presented a  
258 significant gain. In general, the NR2 treatment presented the best result for all shear tests of the  
259 2<sup>nd</sup> glue line.

260 The use of NFC improved the interaction of the adhesive with the wood, with greater  
261 resistance in relation to the control sample. There was an increase of 85,6 % for the NR1  
262 adhesive in the core in the dry shear test. For the NR2 adhesive, the highest gains were for the  
263 face in the dry shear tests (17,18 %) and the core after 72 hours of boiling (44,89 %). NR3  
264 adhesive produced the highest gains for the core shear test after 6 hours of boiling (29,16 %),  
265 while the gains after 72 hours of boiling in the core were 35,71 % and 9,37 % on the face. These

266 results indicate that higher NFC contents improve properties under more severe test conditions  
267 of plywood, while lower NFC contents can be employed to improve panels that will not be  
268 exposed to severe conditions. Despite the improvement in shear strength for the face after 6  
269 hours and the boiling cycle with the addition of NFC, none of the treatments met the  
270 requirements of EN 314-2 (CEN 1993b).

271 The reduction of face shear strength with increased NFC content may have occurred due  
272 to the lower penetration of the adhesive into the veneer because of the increase in the viscosity  
273 of the adhesives. Pre-curing of the adhesive during pre-pressing of the panels may also have  
274 occurred due to the reduction of the gel time with the addition of NFC. Combined effects occur  
275 during the static bending test. Traction, compression and shear stress simultaneously change  
276 when the sample is subjected to the static bending stress. The decrease in shear strength of the  
277 face glue line with increased NFC content influenced the static bending strength, since this is  
278 one of the resistance forces that can cause the increase of the static bending property.

279 Zhang *et al.* (2011) found a 23,6 % increase in static bending property of the urea-  
280 formaldehyde resin (UF) glue line with addition of 1,5 % CNC modified with APTES in the  
281 glue line of plywood panels. CNC values above 1,5 % cause the formation of nanocellulose  
282 clusters that lead to a decline of this property. Eichhorn *et al.* (2010) found significant gains  
283 when 5 % CNF was added to UF adhesive for the production of bonded joints. The addition of  
284 CNF of 0,5 % to 5 % to UF resin allowed a significant gain in stress and strength until composite  
285 failure. The researchers attributed this increase to the absence of cracks, commonly observed  
286 in UF glue lines.

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## CONCLUSIONS

290 The addition of NFC to the adhesive caused an increase in the viscosity and decrease of  
291 the gel time, while the pH remained constant.

292 The application of the nanocellulose caused improvement of the rheological properties of  
293 the adhesive and can decrease the cost of the adhesive.

294 The plywood's specific gravity was not altered with the addition of NFC to the adhesive.

295 There was a reduction in static bending properties for the parallel MOE and MOR and  
296 perpendicular MOR of the panels made with the adhesive with 0,064 % NFC and, for  
297 perpendicular MOE with use of the adhesives with 0,038 % and 0,064 % NFC.

298 All plywood panels conformed with the minimum strength requirements of the European  
299 standard for core glue line shear strength. For the face veneer, only the dry test results were in  
300 accordance with the required shear strength.

301 In general, the best results of the mechanical properties of the panels were obtained with  
302 0,038 % NFC in the adhesive.

303 Since the addition of NFC alters the rheological properties, especially the viscosity, which  
304 in turn interferes with the penetration of the adhesive in the wood, new formulations must be  
305 tested in order to maintain the viscosity commonly employed by plywood manufacturers.

306

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